

Mobil SHC™



# Mobil SHC™ 918 EE

The first turbine oil to meet GE's new energy-efficient turbine oil specification

# Table of contents

1. Mobil SHC™ 918 EE introduction
2. Lowering your cost to produce through energy efficiency
3. GE relationship, rig testing and test stand
4. Field demonstrations and test results
5. GEK 121603 – Energy Efficient Oil for Gas Turbines\*
6. Summary
7. Backup

Section 1:

**Mobil SHC™ 918 EE**

**introduction**



# Introducing breakthrough turbine oil performance

Next-generation Mobil SHC™ 918 EE turbine oil is the first and only oil in the world to meet GE's new rigorous GEK 121603 energy-efficiency specification. It was designed in collaboration with GE to help gas turbine operators:

- Experience energy-efficiency benefits.
- Lower production costs\* while maintaining performance and reliability.
- Lower emissions per megawatt-hour

**Patented formulation is based on Mobil DTE™ 932 GT\*\* technology.**

\*Actual results can vary depending upon the type of equipment used and its maintenance, operating conditions and environment, and any prior lubricant used. The energy efficiency of Mobil SHC™ 918 EE relates solely to the fluid performance when compared to conventional ISO 32 VG turbine oils.

\*\*Mobil DTE™ 932 GT at over 70K hours in GE Frame 7FA – **no varnish, no varnish mitigation**

# Applications

GE Frame 7FA, 7HA multi-shaft and Frame 6FA.01 turbines

- Not for steam turbines or GE Frame 7EA, 5, or 3 gas turbines
- GE Frame 7FAs opportunities approved by GE



Section 2:

# **Lowering your cost to produce through energy efficiency**

# Here's how the savings add up:

In a Frame 7FA.03 169 MW gas turbine operating at 5,000 hours with 38.6% nominal cycle efficiency, Mobil SHC™ 918 EE can deliver:\*

- \$39 K incremental sellable electricity\* (or 136 kW free electricity), or
- \$9,200 in reduced fuel consumption per year\*
- 455 tons in CO2 reduction per year

## Mobil SHC™ 918 EE delivers:



Up to \$48,200  
increased profitability  
per year\*

# Mobil SHC™ 918 EE can deliver:

**\$39,000**

incremental sellable  
electricity per year\*

or

**\$9,200**

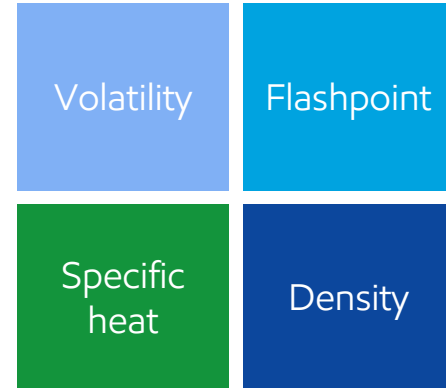
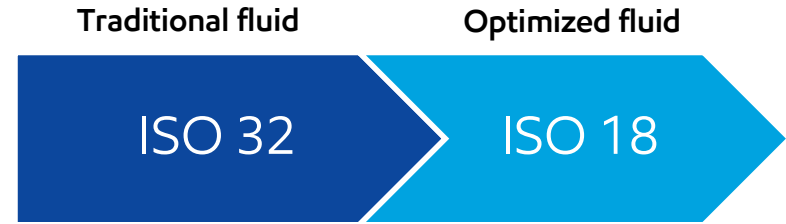
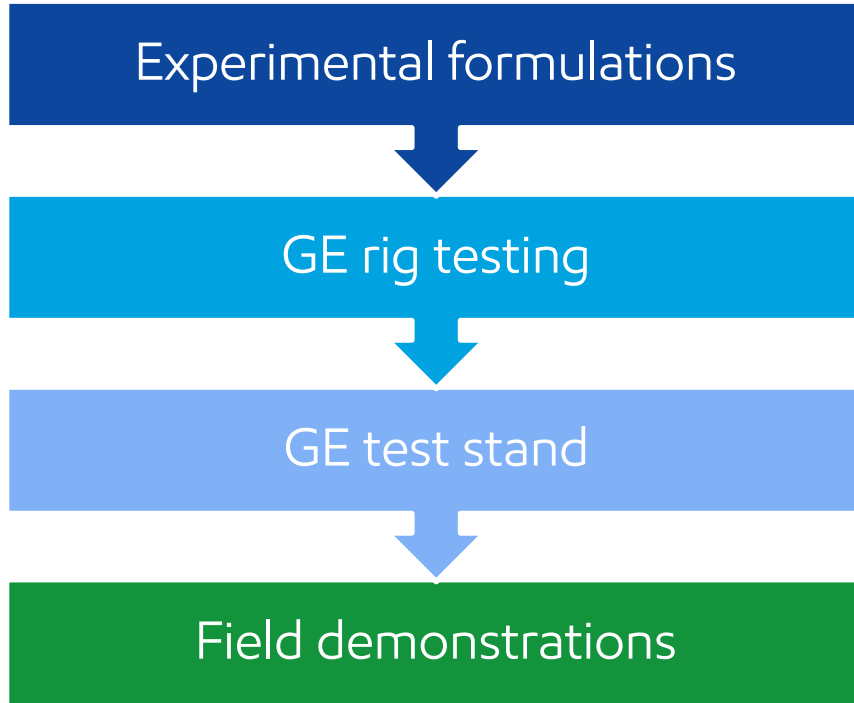
in reduced fuel  
consumption per year\*



Section 3:

# **GE relationship, rig testing and test stand**

# Developed in collaboration with GE



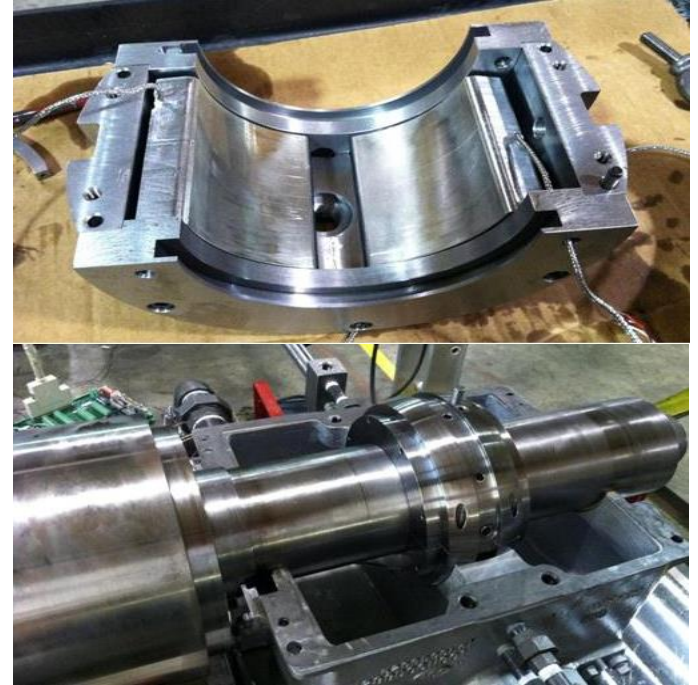
# GE-designed low-loss bearing (LLB) rig

**GE and ExxonMobil collaboration led to low-loss bearing rig testing and protocols (based on ASTM D 7721) to demonstrate bearing efficiency improvement.**

- Tested candidate oil using “A-B-A-B” approach over four days, run at four speeds and six loads
- Scaled-down journal bearing with standard four-tilting pads
- Captured substantial raw data points to conduct statistical analysis

## GE Low-Loss Bearing Test

Approximate 16% bearing efficiency improvement



# GE-designed low-loss bearing (LLB) rig data

A series of A – B – A – B tests were run at varying RPM (four speeds) and loads (six loads). This table represents a comparison of heat loss at one of the four speeds. Test data offers the most representative test speed and loading according to GE.

**VG 32 vs VG 18 at constant oil flow oil and inlet temperature under varying loads**

	Load (PSI)	46.7	75	125	200	300	400	AVG
VG 32	Calculated loss (HP)	39.6	42.3	44.7	45.7	47.9	49.2	44.9
VG 18	Calculated loss (HP)	35.1	36.3	36.2	37.3	39.5	40.8	37.5
Delta	Calculated loss (HP)	4.53	5.96	8.44	8.47	8.36	8.4	8.4
<b>% Delta</b>	<b>Calculated loss (HP)</b>	<b>11.43%</b>	<b>14.09%</b>	<b>18.90%</b>	<b>18.52%</b>	<b>17.46%</b>	<b>17.07%</b>	<b>16.39%</b>

Additional supporting test parameters: Flow (GPM), Oil Inlet and Drain by RTD (F), Brg Metal Temp, Torquemeter Loss (HP)

The table above shows data at 9,550 RPM, which according to GE is the most representative speed with most representative loading at 300 psi.

# GE 7HA test stand results

## Bearing power loss reduction: 16%

- No significant difference in vibration at critical speeds or steady state
- Bearing Metal T showed reduction: 8°F



Section 4:

# **Field demonstrations and test results**

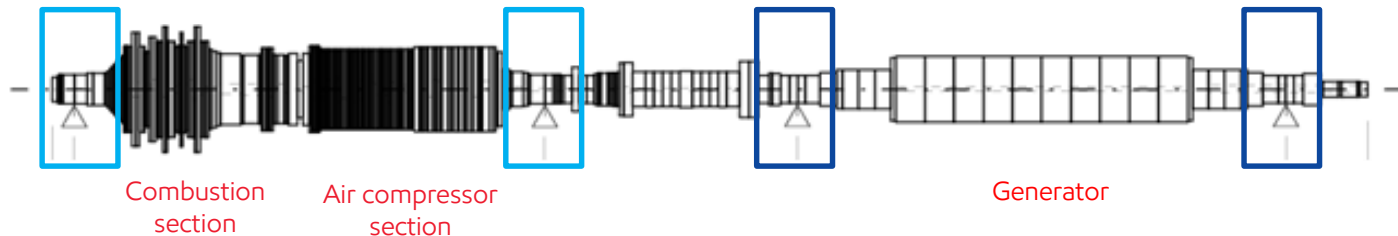
# GE Frame 7FA field demonstration

15% bearing efficiency improvement

15% bearing efficiency improvement

16% bearing efficiency improvement

16% bearing efficiency improvement



**GE 7FA is a four-bearing machine.**

Two generator bearings

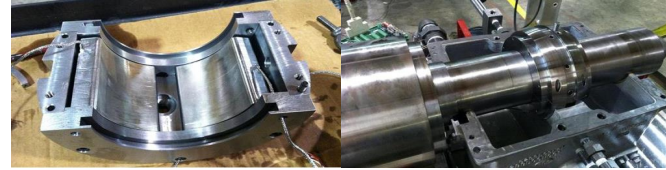
Two gas turbine bearings

Load (MW)	Bearing number	VG 32 Oil			Mobil SHC <sup>®</sup> 918 EE		
		BMT (degrees Fahrenheit)	Oil drain (degrees Fahrenheit)	Power loss (KW)	BMT (degrees Fahrenheit)	Oil drain (degrees Fahrenheit)	Power loss (KW)
168.2	GT No. 1	208	155.8	468	201	151	399
	GT No. 2	187.7	155.9	217	179	151	184
	GEN No. 1	212.1	156.3	103	198	152	90
	GEN No. 2	212	158.3	111	197	152	90
		Sum =		899	Sum =		763
					Delta (KW)		136

# Bearing efficiency test summary

## GE Low-Loss Bearing Test

Approximate 16% bearing efficiency improvement



## GE Test Stand

Approximate 16% bearing efficiency improvement



## GE Frame 7FA Field Demonstration

Approximate 15-16% bearing efficiency improvement



Source: sirgen.com



Mobil SHC™ 918 EE produced a

**.08%**

heat rate reduction\*.

\*This result was based on a field trial. Actual results can vary based on operating conditions and prior lubricant used.



# Field demonstration results

Bearing power losses of 0.5320% can be reduced to 0.4505% — providing a **15-16% bearing efficiency improvement.\***

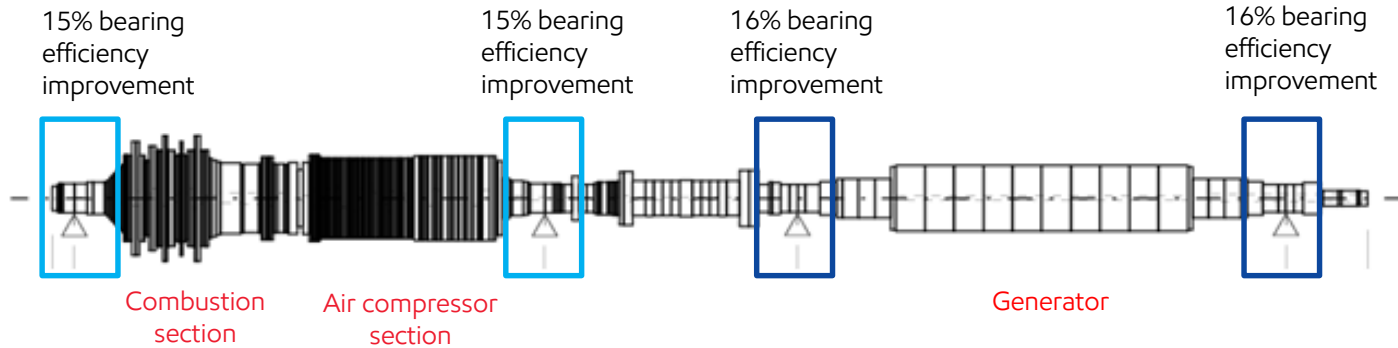
**Field trial for 2+ years in 7FA.03 with no varnish mitigation technology**

## GE Frame 7FA Efficiency Calculator

	<b>P<sub>VG32</sub></b> <b>(HP)</b>	<b>Reduction</b> <b>(%)*</b>	<b>P<sub>VG18</sub></b> <b>(HP)</b>
<b>Gas Turbine</b>			
No. 1 Journal + Thrust	627.6	15.0	533.5
No. 2 Journal	291.0	15.0	247.4
<b>Generator</b>			
Drive End	138.1	16.0	116.0
Collector End	148.9	16.0	125.1
<b>Total (HP) =</b>	<b>1,206</b>		<b>1,022</b>

Additional Power (KW) =	---		136
Bearing Power Losses (%) =	0.5320		0.4505
Heat Rate (Btu/kWh, LHV) =	8839		8832
Heat Rate Improvement (%) =	---		<b>0.08</b>
Machine Output (MW) =	169		169.136
<b>Efficiency Gain (%) =</b>	---		0.0314
Gas Turbine Efficiency (%) =	<b>P<sub>VG32</sub></b> <b>38.6</b>		<b>P<sub>VG18</sub></b> <b>38.6314</b>
Electricity Cost (\$/KW-hr) =	---		<b>0.0567</b>
Hours Operation (hrs/year) =	---		<b>5,000</b>

# GE Frame 7FA field demonstration



**GE 7FA is a four-bearing machine.**

Two generator bearings

Two gas turbine bearings

Baseline gas turbine efficiency = ~38.6%

- Baseline bearing power losses = ~.53%
- Mobil SHC™ 918 EE bearing power losses = ~.45%
- **Bearing power loss delta = 15-16%**

Efficiency impacts:

- Bearing power losses: thermal energy loss due to friction and heat transfer
- Heat rate: thermal energy in divided by electrical energy out (inverse of efficiency)
  - **Lower heat rate = improved energy efficiency (i.e., less fuel)**

# Improved energy efficiency = reduced fuel



## Customer impact:

**Fuel savings** = (Heat rate reduction) X (Operating Hours) X (Natural Gas Price) X (Baseline Output in MW) X (NPV factor\*)

**Fuel savings** = (7.2 Btu/kWh) X (5,000 hours) X (\$2.50/MMBtu) X (169 MW) X (0.005)

**10-year NPV  
fuel savings =  
\$76,000\*\***

Section 5:

# GEK 121603 – Energy Efficient Oil for Gas Turbines\*

\*GEK 121603 – Lubricating Oil Recommendations Energy Efficient Oil for Gas Turbines with Bearing Ambients above 500 degrees Fahrenheit

# Exclusive endorsement

GE created the new GEK 121603 turbine oil specification for energy efficiency. Mobil SHC™ 918 EE is the **only oil** that meets the specification!

Table 1. Recommended Properties – New Oil

Test method	Test	Recommended Value
ASTM D4052	Specific Gravity at 15.6°C	0.76 to 0.88
ASTM D1500	Color	≤2
ASTM D97	Pour Point (°C)	≤-12
ASTM D445	Kinematic Viscosity @ 40°C (centistokes)	16.5 to 20
ASTM D974	Acid Number (mg KOH/g)	≤0.2
ASTM D665	Rust Prevention — B	Pass (4 Hours)
ASTM D92	Flash Point — Cleveland Open Cup (°C)	≥215
ASTM D130	Copper corrosion (3 hour/100°C)	≤1B
ASTM D892	Foam Sequence 1 ml/ml	≤50/0
	Sequence 2 ml/ml	≤50/0
	Sequence 3 ml/ml	≤50/0
ASTM D943	Turbine oil oxidation test (hours)	≥5,000
ASTM D2272	Oxidation Stability by Rotating Vessel (minutes)	≥500
ASTM D2272	Oxidation Stability by Rotating Vessel (modified per ASTM D2272 Appendix XI)	≥85% of time in unmodified test
ASTM D3427	Air Release	≤5
ASTM D2270	Viscosity Index (V I)	≥95
ASTM D5182 or ISO 14635-1	FZG Gear Rig Test Failure Load Stage*	≥8
ASTM D5185	Zinc Content ppm — Spectroscopy	≤5

\*Test is required for geared turbines; may be omitted for non-geared turbines.

**Energy Efficiency claims must be confirmed by GE-approved rig testing and GE-approved gas turbine field demonstration. Geared generators must have confirmed performance in GE-approved gear box manufacturer.**

Section 6:

# Summary

# Mobil SHC™ 918 EE lowers your cost to produce.

- Mobil SHC™ 918 EE , developed in collaboration with GE, delivers energy-efficiency benefits:
  - Resulting in \$76,000 in 10-year NPV savings\*
  - 455 tons in CO2 reduction per year\*

## Make the switch today

Learn more at [mobil.com/efficientturbines](https://mobil.com/efficientturbines)



Section 7:

# Backup



## Experts you can trust

Mobil SHC™ 918 EE is backed by the Mobil Serv™ promise and more than 150 years of ExxonMobil expertise. Mobil Serv experts work with you as committed partners to help you reach your goals.

Tap into best-in-class expertise developed through trusted OEM relationships, groundbreaking research and an extraordinary legacy of lubrication achievements. Contact your sales representative for more information.

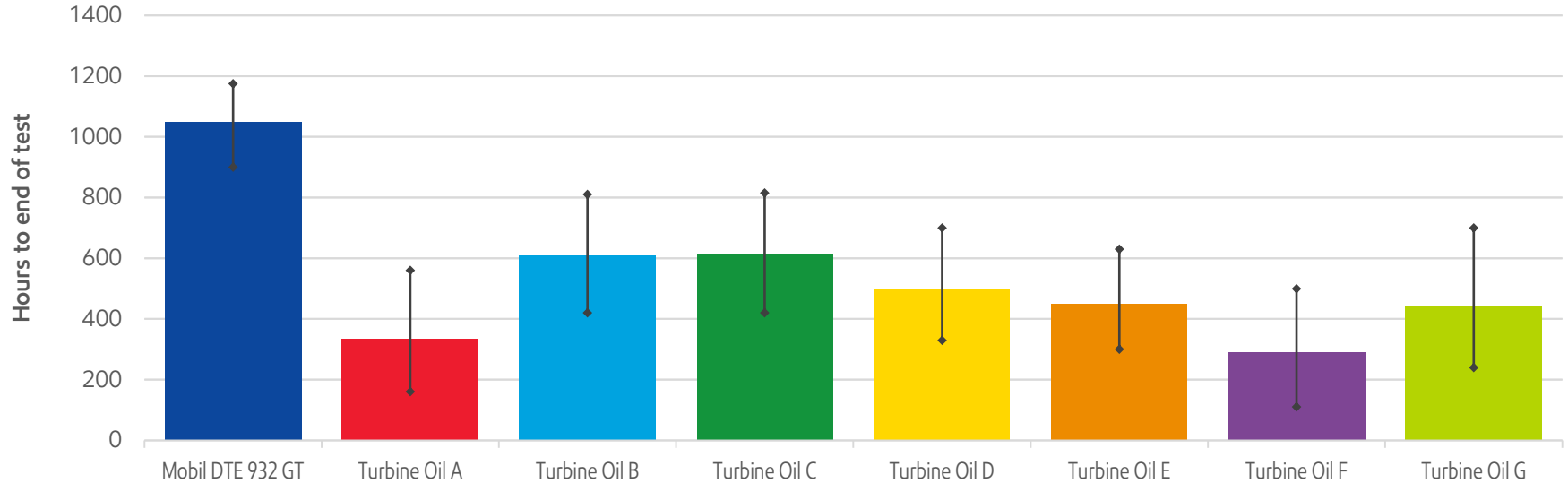


# Mobil SHC™ 918 EE vs. GEK 121603

Test (ASTM)	Method	Units	Min	Max	Mobil SHC 918 EE
D4052	Specific Gravity @ 15.6C		0.76	0.88	0.8371
D1500	Color			2.0	L0.5
D97	Pour Point	°C		-12	-33
D445	Viscosity 40C	cSt	16.5	20	18
D974	Total Acid Number			0.2	0.07
D665	Rust Prevention – B, 4 hour		Pass		Pass
D92	Flash Point (COC)	°C	215		231
D130	Copper Corrosion	Rating		1B	1A
D892	Foaming Tendency Seq 1	mL		50	10
D892	Foam Stability Seq 1	mL		0	0
D892	Foaming Tendency Seq 2	mL		50	10
D892	Foam Stability Seq 2	mL		0	0
D892	Foaming Tendency Seq 3	mL		50	10
D892	Foam Stability Seq 3	mL		0	0
D943	Turbine Oil Oxidation Test	hrs	5000		>10,000
D2272	Oxidation Stability by Rotating Pressure Vessel	minutes	500		2006
D2272	Oxidation Stability by Rotating Pressure Vessel (mod)	minutes	85% of unmodified test		106.7%
D3427	Air Release, Time to 0.2 Pct Air	minutes		5.0	0.7
D2270	Viscosity Index		95		125
D5182	FZG Gear Failure Load Stage*	stage	8		10

# Mobil SHC™ 918 EE based on Mobil DTE™ 932 GT technology

Valve varnish rig test data



Mobil DTE™ 932 GT at over 70K hours in GE Frame 7FA – no varnish, no varnish mitigation technology

# Valve varnish rig test – proprietary

## Evaluates varnish control

- Provides relative assessment of performance of turbine oils under simulated service conditions

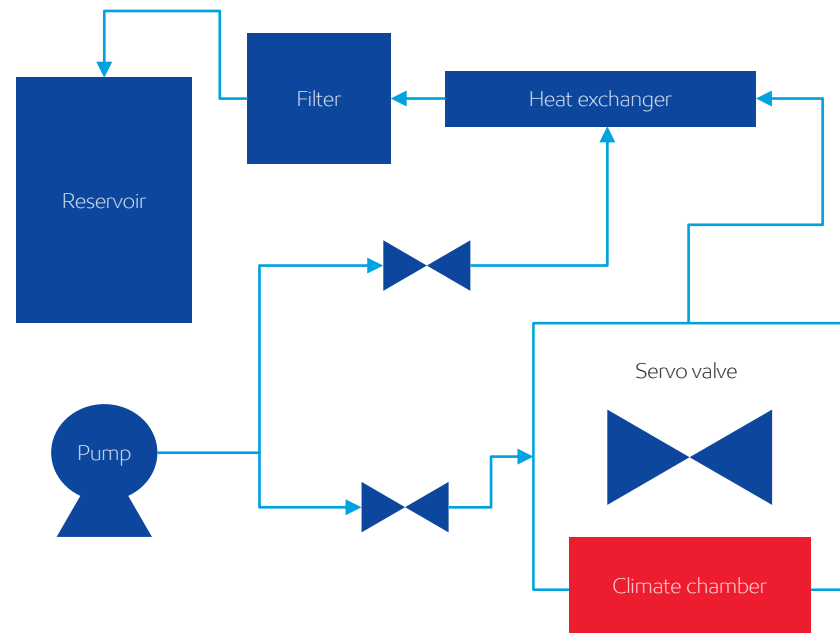
## Rig configuration

- Oil circulation system containing a reservoir, pump, heat exchanger, filter and control valves
- Utilizes cyclic on/off operation to simulate real-world conditions

**Used exclusively by ExxonMobil to help develop high-performing turbine oils**

**More relevant than glassware tests because it replicates real-world conditions**

- Analysis confirms varnish deposits generated in the rig test and in the field are chemically similar.



# Varnish causes unit trips/no-starts

## Inlet Guide Vane (IGV) – Ring and gear

- IGV servo is prone to varnish due to supply tube cooling.
- IGV servo actuates the jackshaft which operates the ring and gear for air flow control.

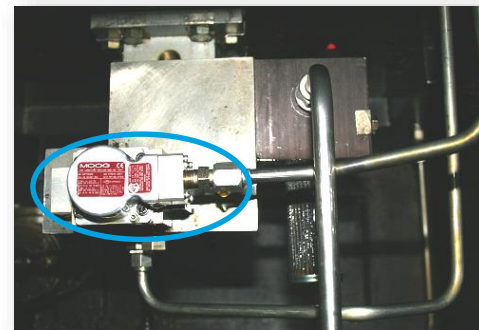


## Servo Valve – Spool



## Gas Ratio Servo

- Air-to-fuel ratio control servo valve sticking can cause unit trips or no-starts.



# Energy efficiency calculations

## GE Low-Loss BRG. Rig, GE Test Stand and field demonstrations

### Test objective

Obtain and compare temperature-based calculated power losses.

### Calculated power losses using the following equation:

$$\text{Calculated Loss (hp)} = c_p \cdot Q \cdot (T_d - T_i) / c_f$$

$c_p$  = Specific Heat (BTU/gal · °F)

$Q$  = Oil Flowrate (gal/min)

$T_d$  = Drain Temperature (°F)

$T_i$  = Inlet Temperature (°F)

$c_f$  = Conversion Factor from BTU/min to hp (42.445)

### Performed complete statistical analysis over full data set

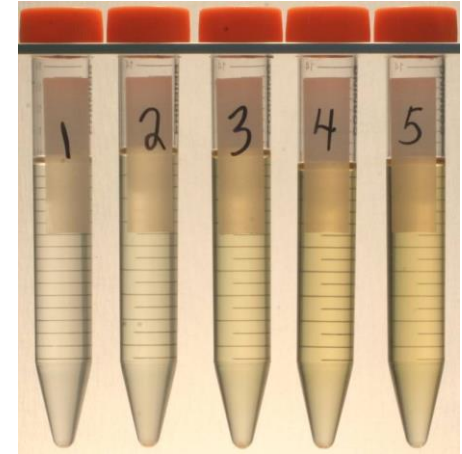
- Understand instrumental variability and validate efficiency conclusions
- Establish reproducibility of data and associated error bars

# Mobil SHC™ 918 EE — compatibility

## Compatibility testing conducted per ASTM D7155 Standard Practice

- Mobil SHC™ 918 EE is fully compatible with:
- Mobil DTE™ 932 GT
- Mobil DTE™ 724
- Mobil DTE™ 832
- Shell VSI 32
- Not compatible with Mobil DTE™ 732
- Hydrogen Absorption similar to Mobil DTE™ 932 GT
- Optimum Mobil SHC™ 918 EE performance is gained through system flushing with Mobil SHC™ 918 EE .

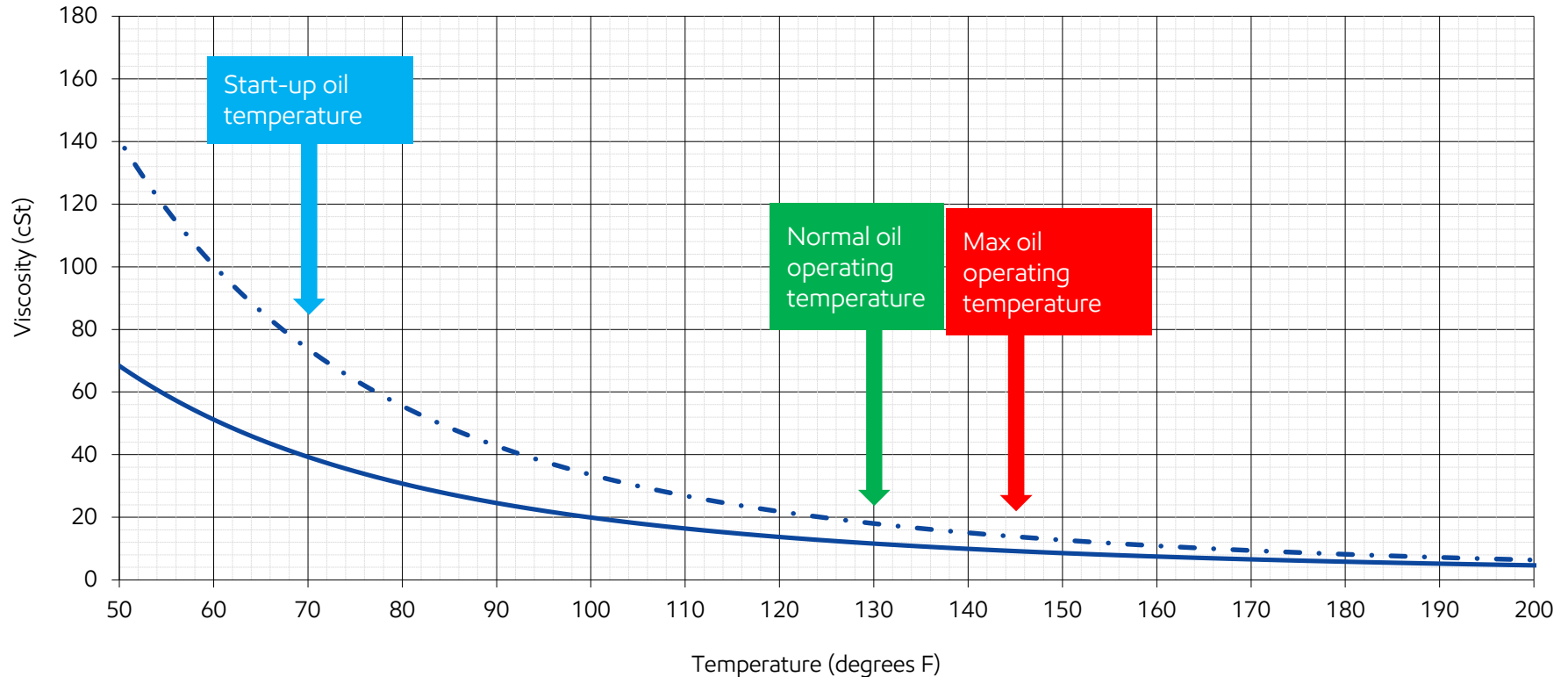
**Freeze/Thaw Storage Stability**



**1 & 2: M-DTE 724    3: 50/50  
4 & 5: M-SHC™918 EE**



# Mobil SHC™ 918 EE viscosity comparison to an ISO 32 oil



# GE Frame 7FA – HP loss comparison

Mobil SHC™ 918 EE requires less horsepower versus water-soluble-based PAG fluids at constant dT (21 degrees Fahrenheit).

**dT is temperature differential between bearing oil inlet and outlet.**

$$\text{Calculated loss (HP)} = (Cp) \cdot (Q) \cdot (T_o - T_i) / 42.445$$

$$\text{Heat Capacity, } Cp = \text{Btu/gal-F}$$

$$Q = \text{gpm}$$

$$T_o/T_i = F$$

## Horsepower loss example comparison (GE 7FA.03):

Mobil DTE™ 732		Mobil SHC™ 918 EE		Water-soluble-based PAG Turbine Oil	
Q=615		Q=615		Q=615	
dT=24		dT=21		dT=21	
Specific heat/BTU/gal-F	3.42	Specific heat/BTU/gal-F	3.33	Specific heat/BTU/gal-F	3.96
HP loss	1188	HP loss	1013	HP loss	1205
HP loss vs DTE 732, %	0	HP loss vs DTE 732, %	14.7%	HP loss vs DTE 732, %	-1.4%

# GE Frame 6FA field demonstration data

## 6FA Noblesville Oil Test

Test date Point	Load (MW)	Bearing Number	Oil inlet (°F)	BMT (°F)	Oil drain (°F)	Oil flow (gpm)	Oil grade (cSt)	Specific heat Btu/gal-°F	Power loss (HP)	Power loss (KW)	
Baseload run		GT no. 1*	130.0	191.6	150.9	190	VG32	3.43	321	239	
3/28/2016	69.5	GT no. 2	130.0	193.6	153.1	60	VG32	3.43	112	84	
3:18 pm		GB HS no. 1	130.0	209.3	179.4	37	VG32	3.43	148	110	
49 °F		GB HS no. 2	130.0	202.5	179.4	37	VG32	3.43	148	110	
		GB LS no. 3	130.0	197.0	179.4	37	VG32	3.43	148	110	
		GB LS no. 4	130.0	194.7	179.4	37	VG32	3.43	148	110	
		GB Mesh	130.0	—	179.4	262	VG32	3.43	1,046	780	
		GEN no. 1	130.0	177.0	156.9	37	VG32	3.43	80	60	
		GEN no. 2	130.0	185.9	160.6	37	VG32	3.43	91	68	
*Inactive thrust = 60 GPM, Active thrust = 70, No. 1 journal = 60 GPM									Sum =	2,242	1,672

BMT VG32	VG18	Delta
191.6	183.1	8.5
193.6	183.8	9.8
209.3	202.8	6.5
202.5	196.3	6.2
197.0	191.0	6.0
194.7	186.1	8.6
—	—	—
177.0	171.1	5.9
185.9	177.7	8.4
avg (°F)		7.5

## 6FA Noblesville Oil Test

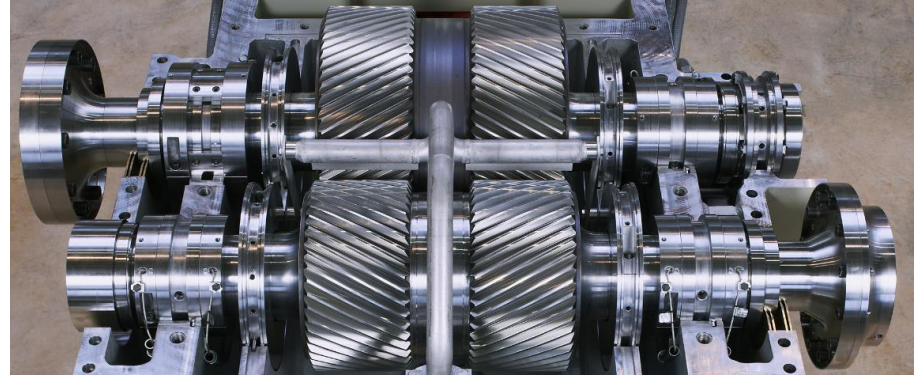
Test date Point	Load (MW)	Bearing Number	Oil inlet (°F)	BMT (°F)	Oil drain (°F)	Oil flow (gpm)	Oil grade (cSt)	Specific heat Btu/gal-°F	Power loss (HP)	Power loss (KW)		
11/17/2017	69	GT no. 1*	130.0	183.1	148.9	190	VG18	3.33	282	210		
3:57 pm		GT no. 2	130.0	183.8	150.2	60	VG18	3.33	95	71		
50 °F		GB HS no. 1	130.0	202.8	178.0	37	VG18	3.33	139	104		
		GB HS no. 2	130.0	196.3	178.0	37	VG18	3.33	139	104		
		GB LS no. 3	130.0	191.0	178.0	37	VG18	3.33	139	104		
		GB LS no. 4	130.0	186.1	178.0	37	VG18	3.33	139	104		
		GB Mesh	130.0	—	178.0	262	VG18	3.33	987	736		
		GEN no. 1	130.0	171.1	152.8	37	VG18	3.33	66	49		
		GEN no. 2	130.0	177.5	156.6	37	VG18	3.33	77	58		
*Inactive thrust = 60 GPM, Active thrust = 70 GPM, No. 1 journal = 60 GPM									Sum =	2,064	1,539	7.9%
										131	Savings (KW)	

GB	1,211	1,151	-5.7%
GT-Gen	451	388	-14.0%

# Gear load capability requirements for GE Frame 6FA

- Gear load protection of FZG (FLS) 8 required
- Renk gear test rig collaboration
- EB Germany supports testing/oil storage and distribution

**Successfully completed Renk gear box testing**



11/8/17

07/30/18

No increase in gear wear since start-up

**Thank you**