

# Polymer Technology in lubrication and approaches to reduce costs in formulations.

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Toronto STLE Chapter, May 15, 2019



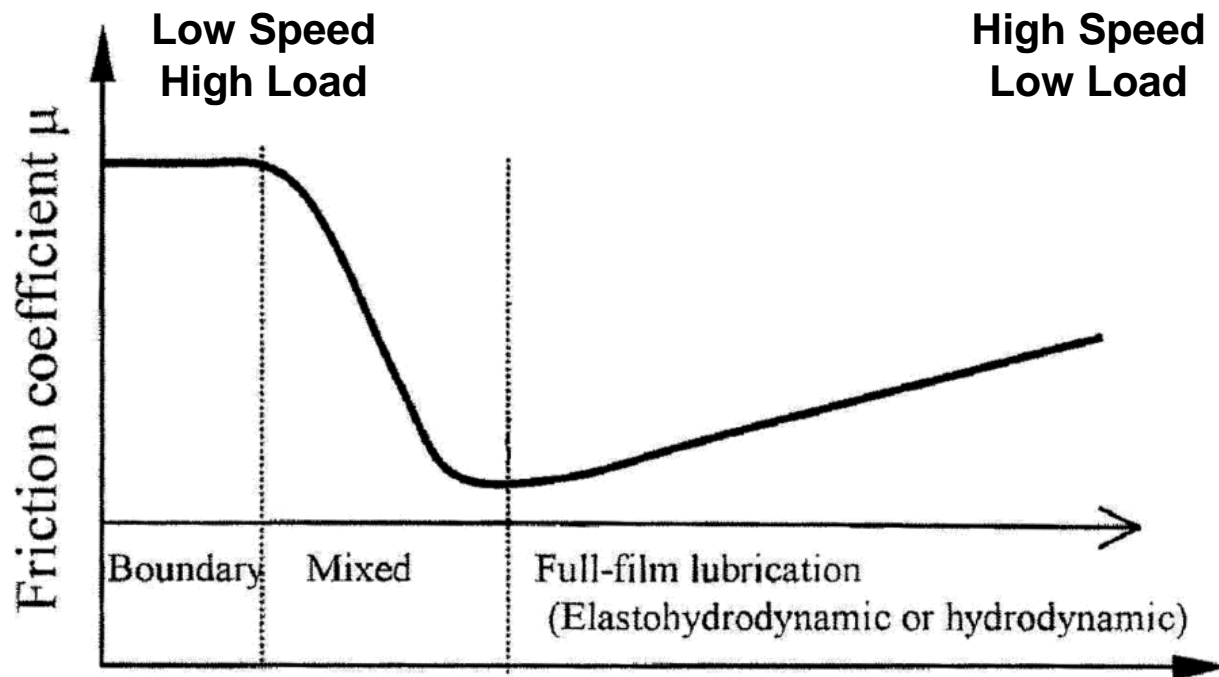
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# **Polymer Technology (VM Fundamentals)**



- Stribeck curve - three regimes of lubrication
  - **Viscosity** of lubricant vs. **Speed / Load** of application



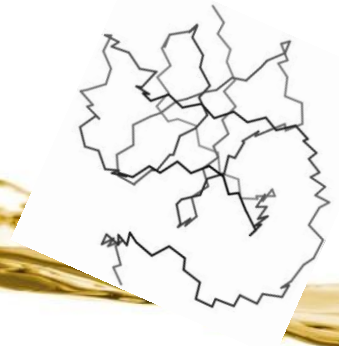
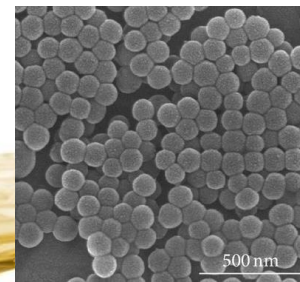
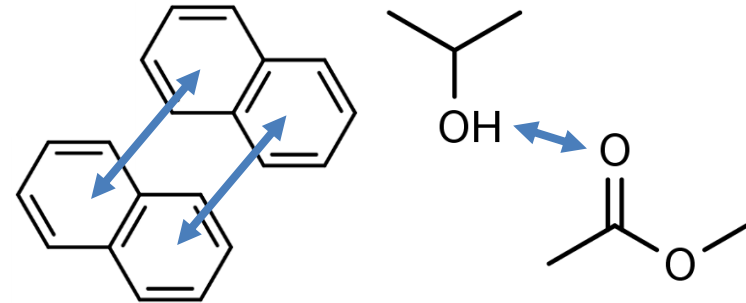
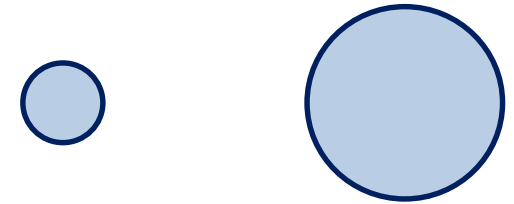
**Viscosity  $\times$  Speed / Load = Hersey Number**

- **Viscosity** is a fluid's resistance to flow

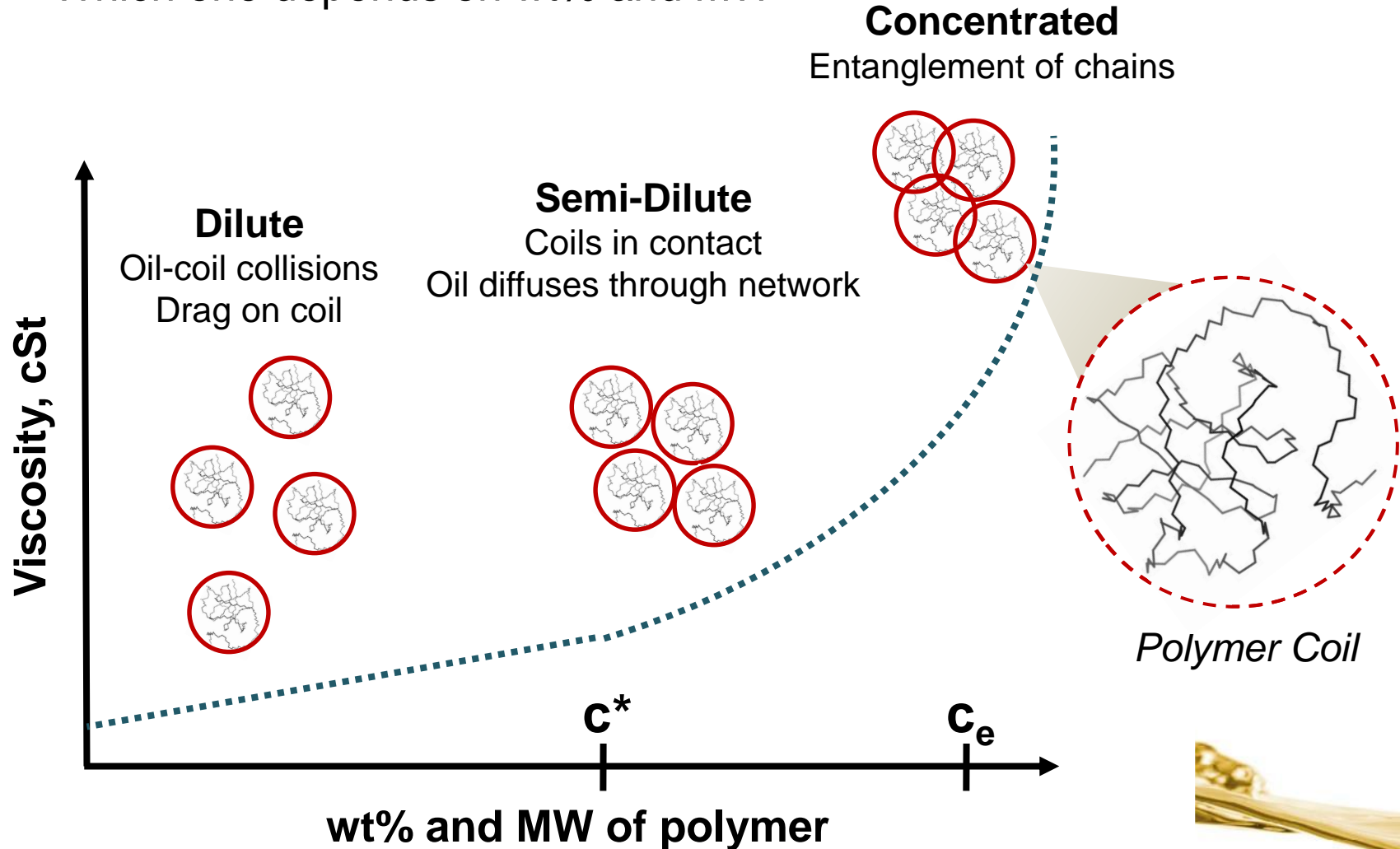
- Size / MW of the fluid

- Attractions (aromatics, esters, hydroxyl)

- Physical obstructions (particles, **polymers**)



- Three regimes of polymer solution behavior
  - Which one depends on wt% and MW



- Why use VM instead of blending oils?
  1. Cheaper high VI
    - Gr.I and naphthenic with VI 140+
  2. Higher viscosity grades
    - Gr. III, synthetic ester
  3. Better low temperature
    - Polymer + light oil vs. heavy oil + light oil
  4. Low visc, high VI formulations possible
    - Low visc base oils tend to be lower VI





- **Viscosity index**
  - Standard Oil 1929
    - Needed a way to standardize visc-temp relationship of crude oils
      - Condense the logarithmic plot of visc-temp into one number
        - VI 100 = paraffinic Pennsylvania crude
- The higher the VI, the lower the change in viscosity with temperature
- Wider operating temperature window for equipment
  - Oil may fall below or above grade with heating/cooling
  - “All Season” / “Multi-grade” / “High VI”

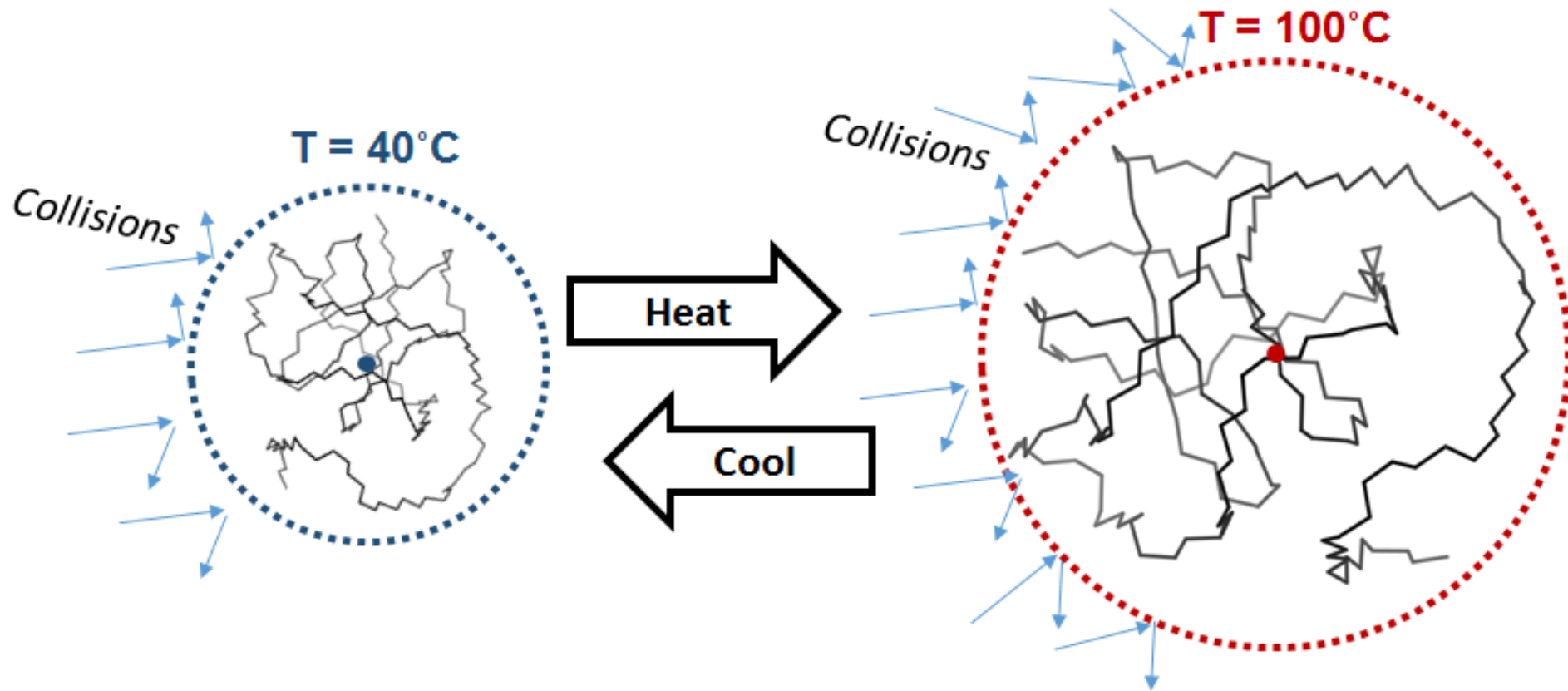




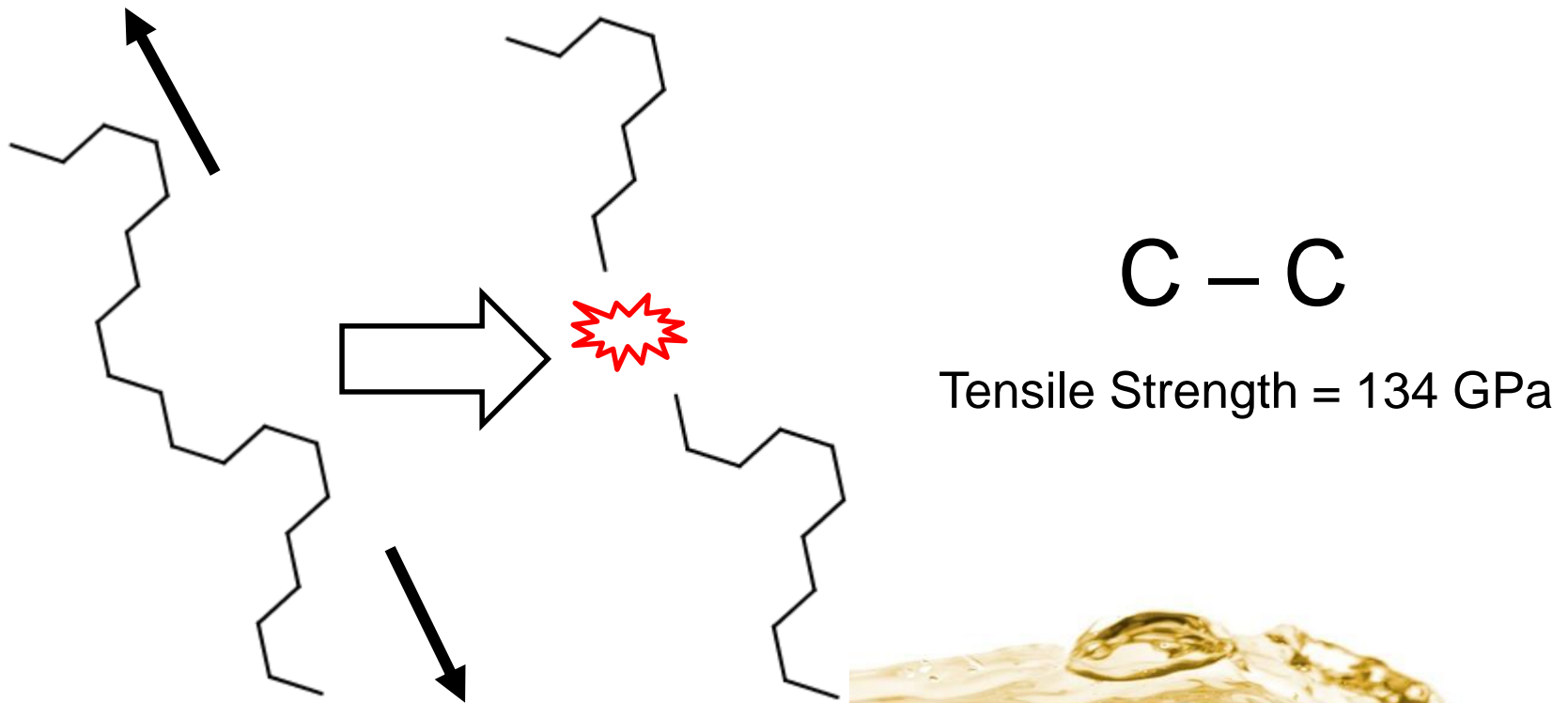
- Wider operating temperature window for equipment
  - “All Season”, “Multi-Grade”, “High VI”



- Some polymers become more soluble at high temp and expand
- The greater the expansion, the larger the obstacle and resistance
  - Relatively higher KV100 = higher VI



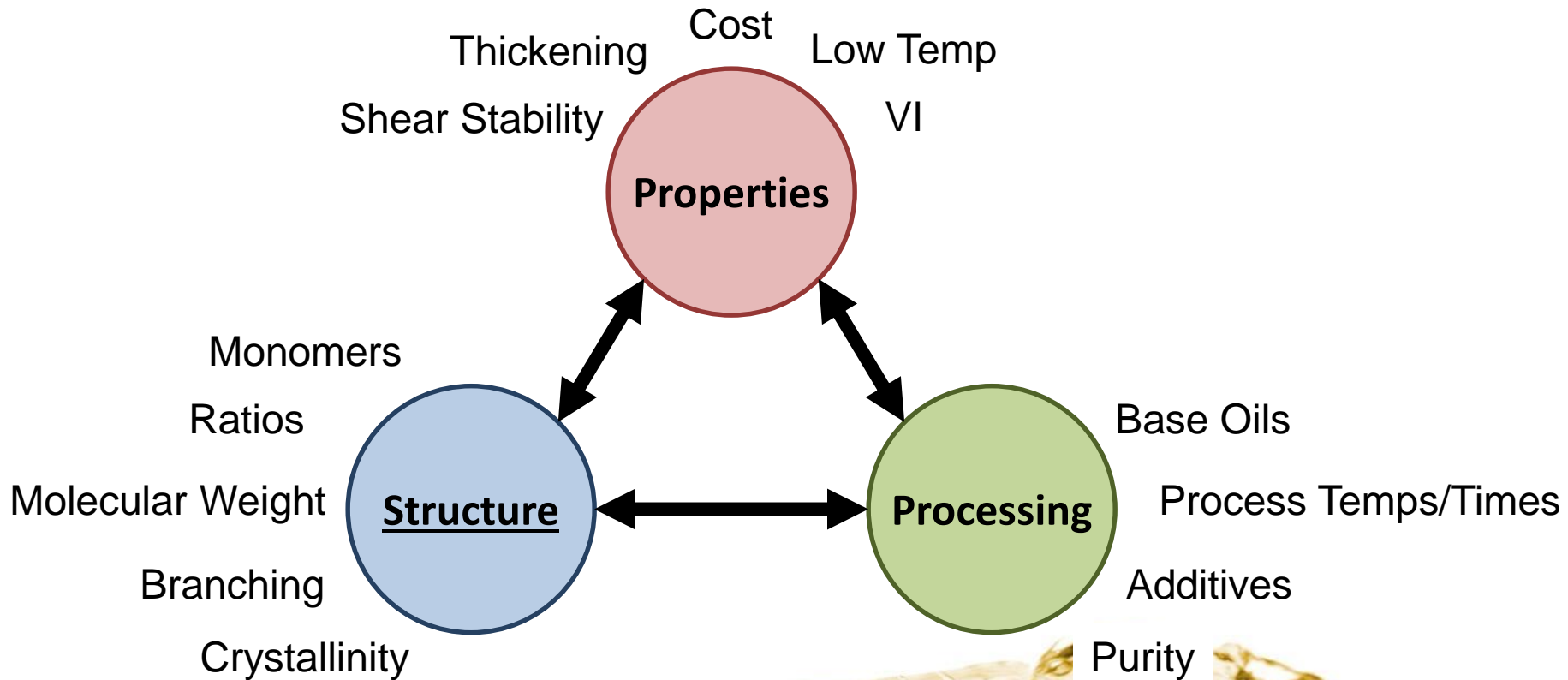
- Mechanical stress on polymer from pressure, cavitation, boundary lub.
  - Carbon-carbon bond ruptures under high stress
    - MW decrease, permanent viscosity loss



- Three main tests of increasing severity:
  - **Engine oil** – ASTM D6278, Kurt-Orbahn / Bosch diesel injector
    - 30 – 250 cycles through diesel injector at 30°C (1min/cycle)
  - **Hydraulic fluids** – ASTM D5621 / D2603, sonic
    - 50W / 23 kHz sonic irradiation at 40°C for 40min
  - **Gear oils** – CEC L-45-A, “20 hour KRL”
    - Tapered roller bearing, 1450 rpm, 5000N load; 60°C for 20 hours



- Why do polymers behave differently? Why are some VM or VII?
  - Material science of polymers



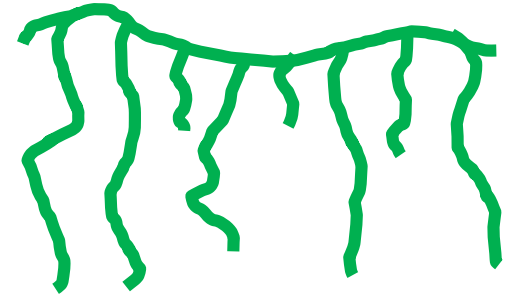
*Linear*



*Star*



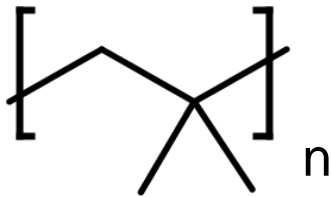
*Comb / Brush*



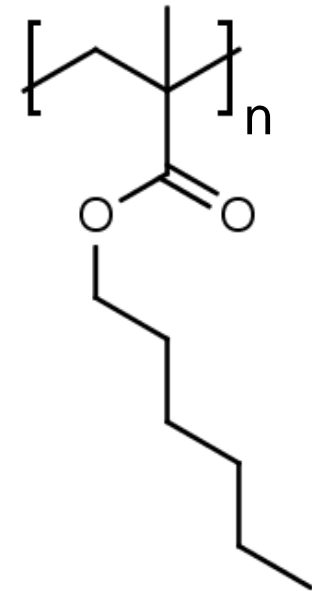


- Hydrocarbon polymers or very high C-H content (PMA)
- Low unsaturation / aromatics

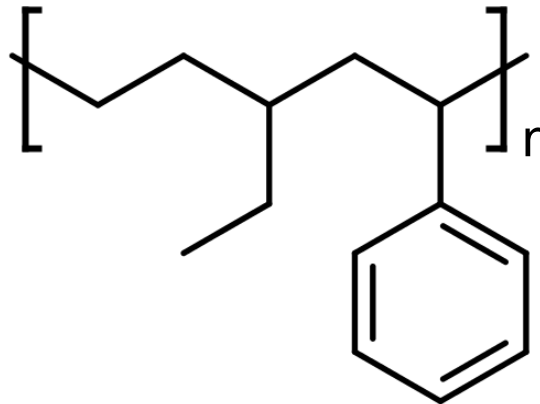
Polyisobutylene (PIB)



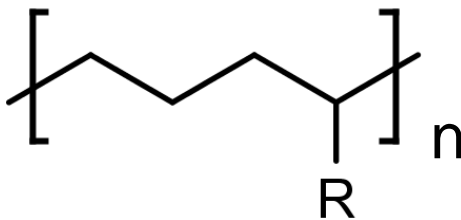
Polymethacrylates (PMA)



Styrene Copolymer



Olefin Copolymer (OCP)





| <b>Chemistry</b>   | <b>Application</b>              | <b>Advantage</b>                                                                                                        | <b>Disadvantage</b>                              |
|--------------------|---------------------------------|-------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------|
| PIB                | Greases, gear, hydraulic fluids | Excellent tackifier<br>Shear stable at low MW                                                                           | Temperature sensitive<br><br>Handling            |
| OCP                | Cost-sensitive, industrial gear | Excellent thickening efficiency<br>Excellent economics<br>Excellent variety and supply<br>Good tackifier                | Poor shear stability<br><br>Poor low temperature |
| PMA                | Gear oil, hydraulic, ATF        | High VI improvement<br>High shear stability<br>Excellent pour point / Brookfield<br>Optional built-in PPD or dispersant | Cost<br><br>High treat                           |
| Styrene Copolymers | Gear oil, hydraulic             | High VI improvement<br>Excellent thickening efficiency<br>Good pour point / Brookfield                                  | Premium pricing<br><br>Limited options           |



Picking a VM / VII for your application depends on several factors:

- **Severity:** EHL/boundary lubrication, high/low temperatures
- **Tier:** Premium vs. fighting grade
- **Use interval:** extended oil change vs. single-pass
- **Region:** Different requirements by country
  
- **Handling:** Solid or liquid VM, maximum viscosity

Biggest concern is shear which will be greatest influence on choice, cost



- A few select tips, tricks, and theory:
  - Designing for shear and shear-in-grade
  - Haze in synthetics
  - Choosing base fluids for higher VI



- How to formulate a product that shears in grade or by a certain %?
  - Less intimidating than it seems to get very good estimates
  - Calculation on paper can save \$\$\$ in shear testing (\$250/per)
- Example:
  - We want to make an ISO 100 product with PAO4.
    - Our customer needs <15% viscosity by KRL shear method.
      - **What viscosity modifier should we use?**



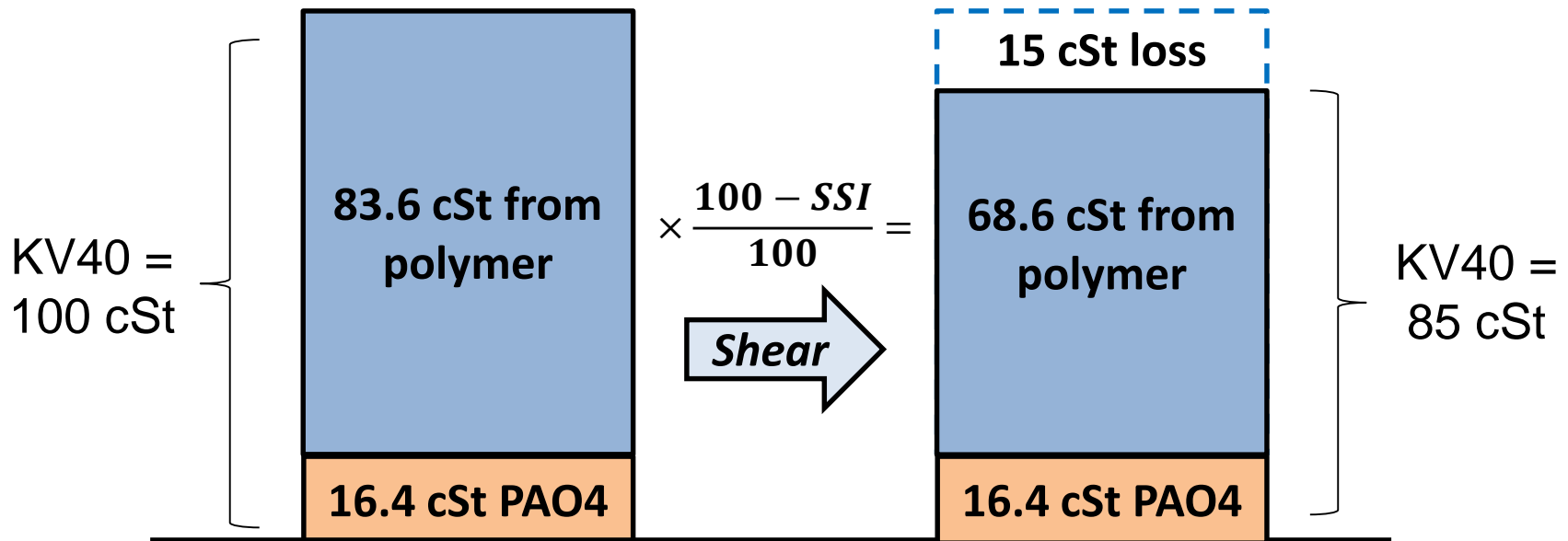
- Most VMs will have at least one SSI reported (Bosch, sonic, KRL)
- That SSI tends to be independent of base fluid, treat rate, or temp.
  - 50 SSI means we'll lose 50% of viscosity we add with that VM
- Knowing *that*, our KV, and **% viscosity from polymer...**
  - Then we can engineer % viscosity loss – quick, accurate, cheap



- Let's say we have an ISO 100 formulation with VM
  - Viscosity of oils + ad paks + polybutene + PAO = **“Base Oil Viscosity”**
  - Product Viscosity – Base Oil Viscosity = **“Viscosity From Polymer”**
    - $100 \text{ cSt product} - 16.4 \text{ cSt of oil} = 83.6 \text{ cSt from polymer}$
    - $83.6 \text{ cSt} / 100 \text{ cSt} = 83.6 \% \text{ viscosity from polymer}$



- Our product viscosity = 100 cSt
- Viscosity from Polymer = 83.6 cSt (83.6%)
  
- What SSI do need to get < 15% loss by KRL?

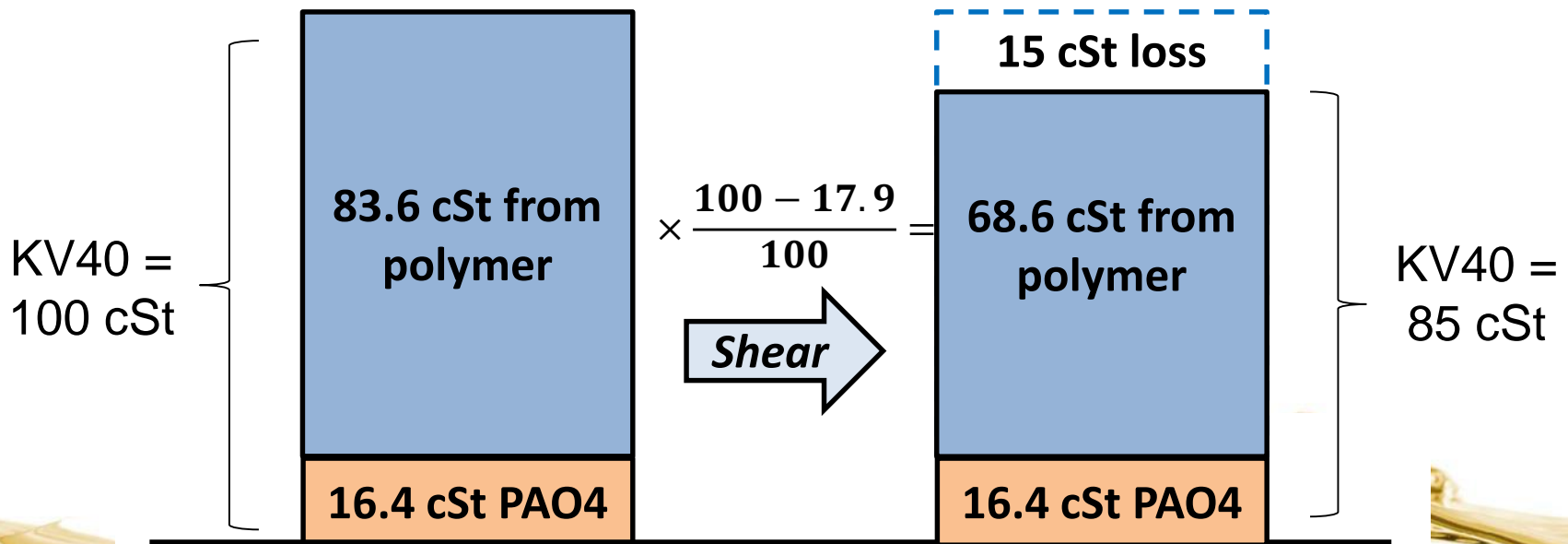




- What SSI do need to get < 15% loss by KRL?

$$\% \text{ Visc Loss} = \% \text{ Visc from Polymer} \times \frac{SSI}{100}$$

$$SSI \text{ Required} = \frac{100 \times \% \text{ Visc Loss}}{\% \text{ Visc from Polymer}} = \frac{100 \times 15}{83.6} = 17.9$$

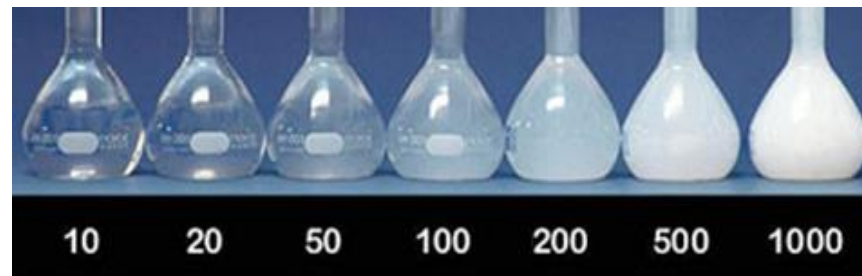


- So we build the ISO 100
  - 31% SSI 15% KRL PMA, VI too high, small volume so PAO pricing not great...
  - Cut back some PMA with a polybutene to save some \$

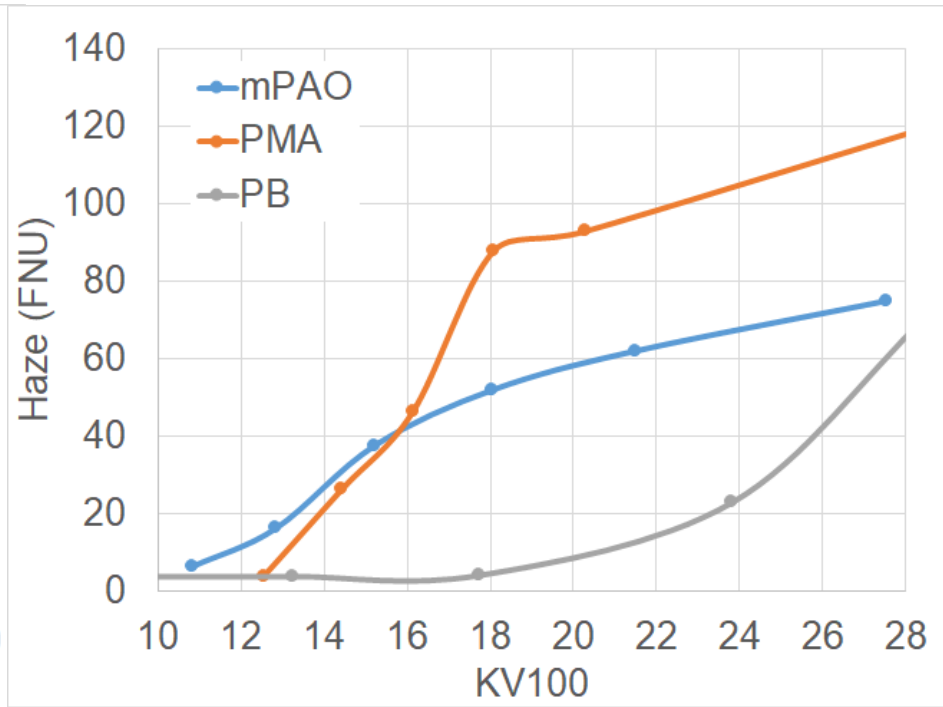
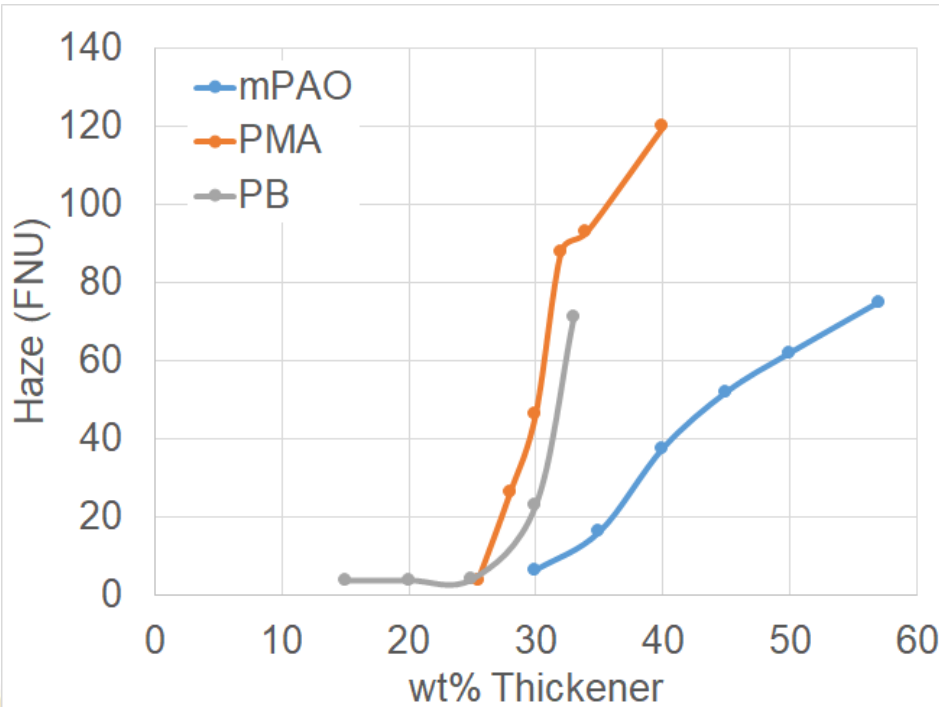
|                     | ISO 100 | ISO 100    |
|---------------------|---------|------------|
| wt%                 | PMA/PAO | PMA/PB/PAO |
| PAO4                | 65.0    | 69.0       |
| <i>PMA 15% SSI</i>  | 31.0    | 20.0       |
| PB 2500 MW          |         | 7.0        |
| Ad Pak              | 4.0     | 4.0        |
| <b>KV40</b>         | 100.6   | 100        |
| <b>KV100</b>        | 17.0    | 15.5       |
| <b>VI</b>           | 184     | 164        |
| <b>\$/lb, rough</b> | \$2.36  | \$2.07     |

- Great! But now something changes...
  - We start seeing **haze** upon standing
  - Low temp viscosities and pour points got worse

- Common in semi/full synthetics with high wt% shear stable VM
  - Low solvency base oil made worse by replacing oil with polymer
    - Higher MW, worse solvency
- *What are the conditions to cause haze?*
  - Study with turbidity meter
    - Haze measured for after -20C freeze/thaw
      - <10 FNU (Formazin Nephelometric Units) haze ideal; 20+ is visible to the eye
  - 0 – 60% PMA, PB, or mPAO in PAO4 with GL-5 ad pak



- Best strategy
  - Limit PMA to < 25wt% and mPAO < 30wt% (likely 13-14 cSt)
  - Get the rest of your viscosity from PB
  - No ester required!



- Additive packages, as a whole, don't haze
  - It may only be a few specific components that haze or precipitate
    - AW / EP / FM / CI / AO / dispersant / detergent / defoamer, etc.
      - Ionic or polar versus non-polar, low solvency PAO
- Functional performed another haze screening with individual components
  - PMA/PB/PAO blend at 75W140 visc, -54C freeze/thaw



- 5 components found to cause haze/drop-out in the 75W140 test formula
  - Visual inspection didn't always agree with turbidity meter

| Trial | Chemistry                   | Treat | Role                      | FNU Haze | Visual      |
|-------|-----------------------------|-------|---------------------------|----------|-------------|
| A     | -control-                   | N/A   | <control>                 | 0        | Clear       |
| B     | Alkyl triazole              | 0.1%  | Corrosion inhibitor       | 10.6     | Clear       |
| C     | Mb dithiocarbamate          | 3.0%  | Friction modifier         | 2.92     | Clear       |
| D     | Aromatic amine              | 1.0%  | Antioxidant               | 1.43     | <b>Haze</b> |
| E     | Ashless dithiocarbamate     | 1.5%  | Ashless friction modifier | 1.62     | Clear       |
| F     | Amine phosphate             | 1.0%  | Corrosion inhibitor       | 4.55     | Clear       |
| G     | Overbased calcium sulfonate | 1.0%  | Detergent                 | 15.7     | <b>Haze</b> |
| H     | PIBSI                       | 1.0%  | Dispersant                | 0.8      | <b>Haze</b> |
| I     | Dialkyl pentasulfide        | 1.0%  | Active sulfur EP          | 0        | Clear       |
| J     | Sulfurized ester            | 1.0%  | Inactive sulfur AW        | 1.15     | Clear*      |
| K     | PAG defoamer                | 0.2%  | PEG Defoamer              | 2.7      | <b>Haze</b> |
| L     | Acrylate defoamer           | 0.2%  | Acrylate Defoamer         | 1.3      | Clear       |

- Discrepancy between measured haze vs. visual inspection
- Worst haze: from D > G, H > K; delayed separation with J after one month



- The five components that hazed are quite standard in ad paks – what now?
  - Optimize PMA/PAO/PB blend for better solvency – previously discussed
  - Add ester (10-20wt) to solubilize the incompatibles
  - If you formulate ad pak from scratch, find lower polarity alternatives
  - If you buy ad pak, some ad paks available specific for synthetics





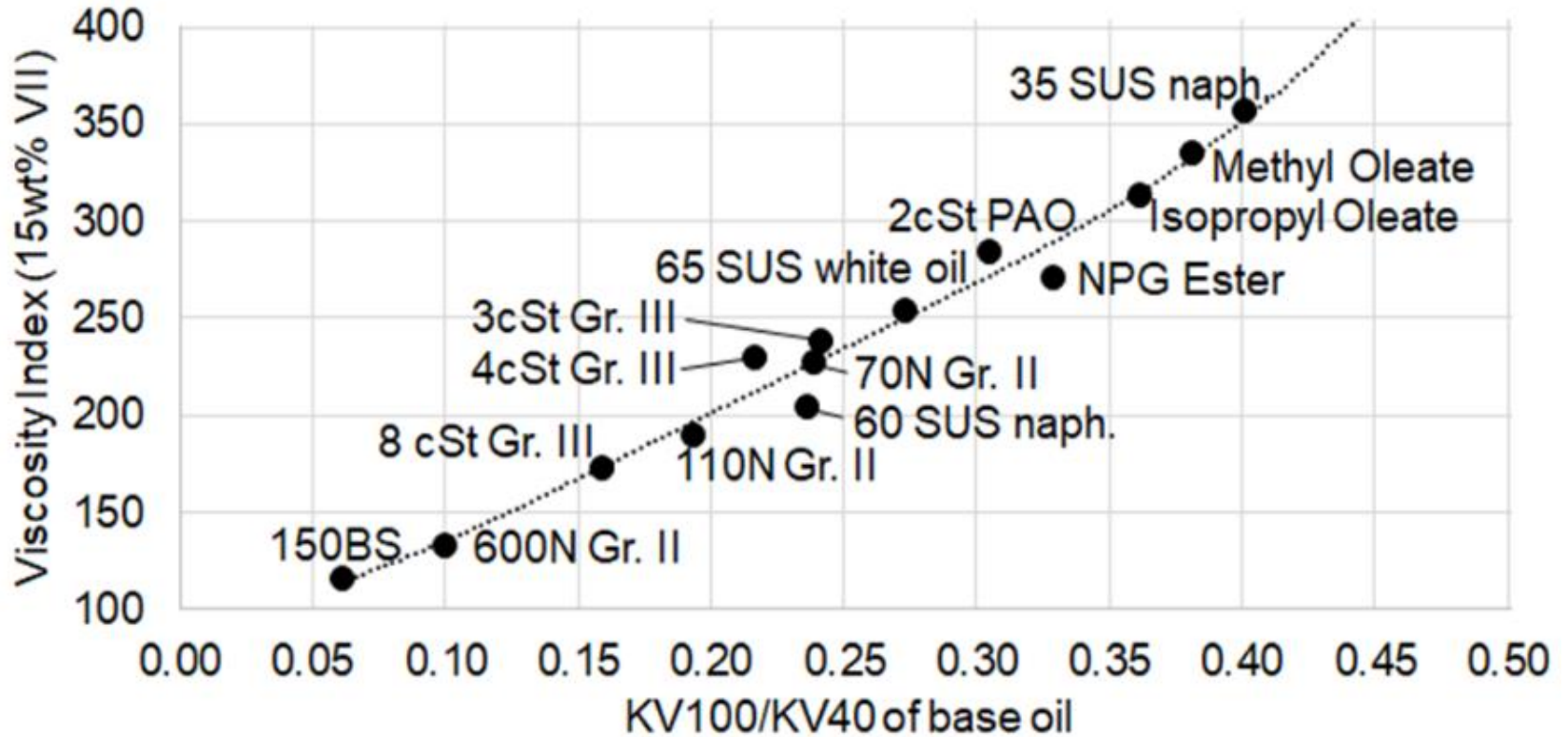
- At that rate, maybe the answer is to go back to higher solvency paraffinics
  - Can you still get high VI without synthetics? *Yes, with the right oil*

| <b>Base Fluid</b> | <b>Viscosity Index<br/>w/ 15% PMA SSI 35%</b> |
|-------------------|-----------------------------------------------|
| D-Limonene        | 572                                           |
| 35 SUS naph. oil  | 357                                           |
| Methyl oleate     | 335                                           |
| Isopropyl oleate  | 313                                           |
| PAO2              | 284                                           |
| C9 NPG Ester      | 271                                           |
| 65 SUS white oil  | 254                                           |
| 3 cSt Gr. III     | 238                                           |
| 4 cSt Gr. III     | 230                                           |
| 70N Gr. II        | 227                                           |
| 60 SUS naph. oil  | 204                                           |
| 110N Gr. II       | 190                                           |
| 8 cSt. Gr. III    | 173                                           |
| 600N Gr. II       | 133                                           |
| 150BS             | 116                                           |

*What's the correlation here?  
Is it high starting VI?  
Low viscosity?  
Synthetic status?*



- Best predictor is the KV100 to KV40 ratio
  - These fluids due to tend to be thinner oils requiring more stable VM



- Designing for shear
  - SSI is a key parameter in designing shear stable formulations
  - Back of envelope calculation is quite easy, accurate
  - Helps make decisions about base oil viscosity, VM, etc.
- Hazy synthetics
  - Low solvency oil + high wt% polymer + polar additives
  - Possible to optimize for clarity without ester
- Very high VI
  - Look at the KV100/KV40 ratio of your base oil blend when VI is low

